

**LOAD FLOW STUDIES ON NIGERIA 330KV NATIONAL GRID SYSTEM, USING
NEWTON-RAPHSON'S METHOD**

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Abstract

Reactive power and voltage control constitute part of the major challenges in power system industry. Compensation in power system is very essential to eradicate the problem of constant power failure and outage in Nigeria power system. In this paper, the Nigerian 330KV, 30-bus system network is considered. Newton-Raphson's solution method was employed to carry out the analysis because of its sparsity, fast convergence and simplicity attributes compared to other solution methods. Using the relevant data, MATLAB/SIMULINK software was used to carry out the simulation analysis and the results obtained showed that bus voltages outside the statutory limit of $0.95 \leq V_i \leq 1.05$ p.u are: bus 14 (Jos) with value of 0.9359 p.u, bus 17 (Gombe) 0.9175 p.u, bus 19 (Maiduguri) 0.9106 p.u, bus 22 (Kano) 0.8849 p.u, bus 28 (Berni -Kebbi) -0.734 p.u, bus 3 (Okpai) 1.090 p.u and bus 29 (Kaduna) 0.9880 p.u while bus 30 (Makurdi) gave the value 0.8247 p.u under normal uncompensated condition.

Keywords: Nigerian 330KV network, Newton-Raphson's method, compensation, reactive power and voltage control.

1.0 Introduction

The Nigerian power network, like many practical system in developing countries, consists of a few generating stations mostly sited in remote locations near the raw fuel sources which are usually connected to the load centres by long transmission lines [1]. Generation, Transmission, Distribution and marketing of electricity in Nigeria are the statutory functions of the National Electric Power Authority (NEPA), now known as (GENCO-TRANSYSCO-DISCO).

Presently, the national electricity grid or the 330KV network consists of nine (9) generating stations, comprising three (3) hydro and six (6) thermal with a total installed generating

capacity of 6500MW [1]. The thermal stations are mainly in the southern part of the country located at Afam, Okpai, Delta (Ughelli), Egbin and Sapele. The Hydro electric power stations are in the country's middle belt and are located at Kainji, Jebba, and Shiroro [2]. The transmission network is made up of 5000km of 330KV lines, 6000Km of 132KV lines which include: New-Haven to Oji River, New-Haven to Nkalagu, New-Haven to Abakaliki, New-Haven to Otukpo/Yandev for Enugu sub-Region; others are: 23km of 330/132KV sub-station and 91km of 132/33KV sub-stations. The distribution sector is comprised of 23,735km of 33KV lines, 19,226km of 11KV lines and 679km of 33/11KV substations. There are also 1,790 distribution transformers and 680 injection substations [1].

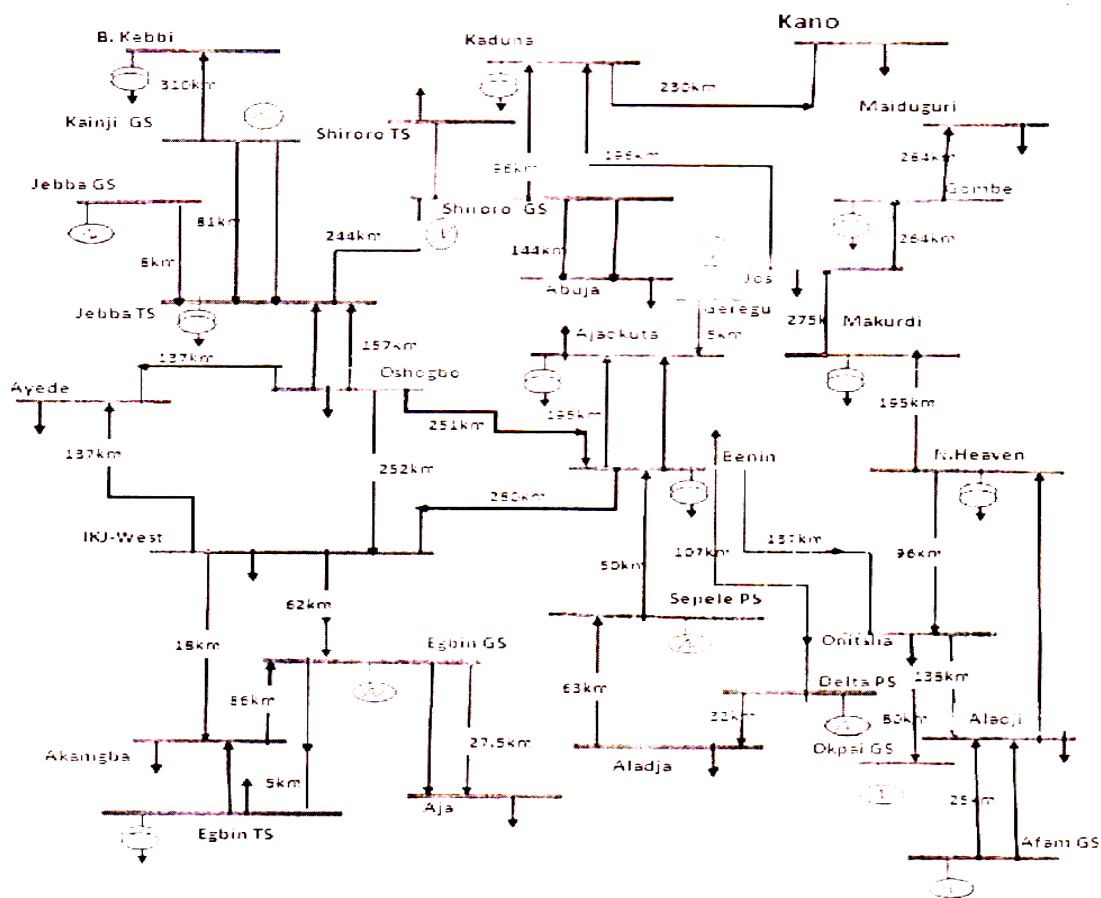


Figure 1: Line Diagram of Nigeria 330KV 30 Bus Interconnected Network.

1.1 What Informed This Research

Although the installed capacity of the existing power stations is 6500MW, the maximum load ever recorded was 4,000MW. Presently, most of the generating units have broken down due to limited available resources to carryout the needed maintenance. The transmission lines are

radial and overloaded. The switch gears are obsolete while power transformers have not been maintained for a long time.

Again, the present installed generating capacity is about 6500MW and maximum generation of 4000MW for a population of about 160 million. This indeed is grossly inadequate to meet the demand of electricity consumers [3]. The current projected capacity that needs to be injected into the system is estimated at 10,000MW which is hoped to come in through the Independent Power Producers (IPPS), as soon as deregulation of electricity supply industry is successfully achieved [3].

And finally massive injection of funds is needed to expand the distribution and transmission networks to adequately transport the power generated to consumers.

The existing generating stations in the country are shown in Table 1 and those under construction are shown in Table 2.

Table 1: Existing Generating Stations in the Country

| S/No | Power station name | Location/ State | Status | Capacity (MW) |
|-------------------------|------------------------------|-----------------|-----------|---------------|
| 1. | Egbin Thermal Power Station | Lagos | Operating | 1320 |
| 2. | Afam Thermal Power Station | Rivers | Operating | 969.6 |
| 3. | Sapele Thermal Power Station | Delta | Operating | 1020 |
| 4. | Ijora Thermal Power Station | Lagos | Operating | 40 |
| 5. | Delta Thermal Power Station | Delta | Operating | 912 |
| 6. | Kainji Hydro Power Station | Niger | Operating | 760 |
| 7. | Jebba Hydro Power Station | Niger | Operating | 578 |
| 8. | Shiroro Hydro Power Station | Niger | Operating | 600 |
| 9. | AES Thermal Power Station | Lagos | Operating | 300 |
| TOTAL CAPACITY = | | | | 6500 |

Table 2: Power Stations/Plants under Construction or Expansion.

| S/N | Name | State |
|-------------------------------------|--------------------------|---------|
| 1. | Eyeon | Edo |
| 2. | Sapele (under expansion) | Delta |
| 3. | Omoku | Rivers |
| 4. | Egbema | Rivers |
| 5. | GbaranUbic | Beyelsa |
| 6. | Onne | Rivers |
| Proposed Hydro Power Plant | | |
| 1. | Dadinkowa | Gombe |
| Proposed Biomass Power Plant | | |
| 1. | Ikeja | Lagos |

2.0 Data Collection from Transmission Company of Nigeria (TCN)

The bus and line data were obtained from TCN based on 2008 – 2010 daily operational reports of GENCO – TRANSYSCO-DISCO, National Control Centre (NCC) Oshogbo. Access to these data online was very difficult, Kudoes to TCN for timely intervention and assistance. The raw data as obtained from TCN are displayed in Tables 3 and 4.

Table 3: Bus Data for 330KV Lines.

| S/No | Bus Name | Generation | | Load | | V | Angle | Remark |
|------|------------------|------------|---------|---------|---------|-------|--------|----------|
| | | P(MW) | Q(Mvar) | P(MW) | Q(Mvar) | Volt | Degree | |
| 1 | Egbin-Gs (slack) | 0.00 | 0.00 | 0.00 | 0.00 | 1.020 | 0.00 | PV Bus |
| 2 | Delta – Ps | 0.00 | 0.00 | 4.00 | -10.00 | 1.000 | 0.00 | PV Bus |
| 3 | Okpai – Ps | 300.00 | 40.00 | 0.00 | 0.00 | 1.040 | 0.00 | PV Bus |
| 4 | SAP/PS | 0.00 | 0.00 | 140.00 | 30.00 | 1.000 | 0.00 | PV Bus |
| 5 | Afam – Gs | 0.00 | 0.00 | 90.00 | 30.00 | 1.000 | 0.00 | PV Bus |
| 6 | Jebba – Gs | 20.00 | 0.00 | 160.00 | 70.00 | 1.040 | 0.00 | PV Bus |
| 7 | Kainji – Gs | 400.00 | 60.00 | 0.00 | 0.00 | 1.000 | 0.00 | PV Bus |
| 8 | Shiroro – Ps | 0.00 | 0.00 | 150.00 | 70.00 | 1.000 | 0.00 | PV Bus |
| 9 | Geregu (Ps) | 0.00 | 0.00 | 300.00 | 90.00 | 1.000 | 0.00 | PV Bus |
| 10 | Oshogbo | 0.00 | 0.00 | 120.370 | 61.650 | 1.020 | 0.00 | Load Bus |
| 11 | Benin | 150.00 | 50.00 | 160.56 | 82.240 | 1.00 | 0.00 | Load |

| | | | | | | | | |
|----|--------------------|--------|--------|--------|---------|------|------|-------------|
| | | | | 0 | | 0 | | Bus |
| 12 | Ikeja-West | 0.00 | 0.00 | 334.00 | 171.110 | 1.00 | 0.00 | Load Bus |
| 13 | Ayede | 0.00 | 0.00 | 176.65 | 90.490 | 1.00 | 0.00 | Load Bus |
| 14 | Jos | 0.00 | 0.00 | 82.230 | 42.129 | 1.00 | 0.00 | Load Bus |
| 15 | Onitsha | 0.00 | 0.00 | 130.51 | 66.860 | 1.00 | 0.00 | Load Bus |
| 16 | Akangba | 0.00 | 0.00 | 233.37 | 119.560 | 1.00 | 0.00 | Load Bus |
| 17 | Gombe | 0.00 | 0.00 | 74.480 | 38.140 | 1.00 | 0.00 | Load Bus |
| 18 | Abuja (Katampe) | 280.00 | 45.00 | 200.00 | 102.440 | 1.03 | 0.00 | Load Bus |
| 19 | Maiduguri | 0.00 | 0.00 | 10.00 | 5.110 | 1.00 | 0.00 | Load Bus |
| 20 | EgbinTs | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | Load Bus |
| 21 | Aladja | 240.00 | 55.00 | 47.997 | 24.589 | 1.02 | 0.00 | Load Bus |
| 22 | Kano | 700.00 | 68.00 | 252.45 | 129.330 | 1.05 | 0.00 | Load Bus |
| 23 | Aja | 0.00 | 0.00 | 119.99 | 61.477 | 1.00 | 0.00 | Load Bus |
| 24 | Ajokuta | 180.00 | 0.00 | 63.220 | 32.380 | 1.04 | 0.00 | Load Bus |
| 25 | New Haven | 0.00 | 0.00 | 113.05 | 57.910 | 1.00 | 0.00 | Load Bus |
| 26 | Alaoji | 190.00 | -35.00 | 163.95 | 83.90 | 1.01 | 0.00 | Load Bus |
| 27 | Jebba – Ts | 150.00 | 51.00 | 7.440 | 3.790 | 1.03 | 0.00 | Load |

| | | | | | | | | |
|----|---------------|--------|-------|--------|--------|------|------|------|
| | | | | | | 0 | | Bus |
| 28 | Benin – kebbi | 130.00 | 80.00 | 69.990 | 35.850 | 1.02 | 0.00 | Load |
| | | | | | | 0 | | Bus |
| 29 | Kaduna | 0.00 | 0.00 | 149.77 | 76.720 | 1.00 | 0.00 | Load |
| | | | | | | 0 | | Bus |
| 30 | Makurdi | 0.00 | 0.00 | 73.070 | 37.430 | 1.00 | 0.00 | Load |
| | | | | | | 0 | | Bus |

Source: TCN National Control Centre Oshogbo Daily Operational Report, 2008 – 2010.

Table 4: Transmission line Data for 330KV Lines

| | | | | | |
|---------|---------|--------|--------|--------|--------|
| 16.0000 | 12.0000 | 0.0006 | 0.0051 | 0.0650 | 1.0000 |
| 12.0000 | 1.0000 | 0.0022 | 0.0172 | 0.2570 | 1.0000 |
| 12.0000 | 11.0000 | 0.0101 | 0.0799 | 1.1620 | 1.0000 |
| 12.0000 | 13.0000 | 0.0049 | 0.0416 | 0.5210 | 1.0000 |
| 13.0000 | 10.0000 | 0.0041 | 0.0349 | 0.4370 | 1.0000 |
| 10.0000 | 11.0000 | 0.0089 | 0.0763 | 0.9540 | 1.0000 |
| 10.0000 | 27.0000 | 0.0056 | 0.4770 | 0.5970 | 1.0000 |
| 12.0000 | 6.0000 | 0.0056 | 0.4770 | 0.5970 | 1.0000 |
| 27.0000 | 8.0000 | 0.0087 | 0.0742 | 0.9270 | 1.0000 |
| 27.0000 | 7.0000 | 0.0022 | 0.0246 | 0.3080 | 1.0000 |
| 7.0000 | 28.0000 | 0.0111 | 0.9420 | 1.1780 | 1.0000 |
| 8.0000 | 29.0000 | 0.0034 | 0.0292 | 0.3640 | 1.0000 |
| 29.0000 | 22.0000 | 0.0082 | 0.0899 | 0.8740 | 1.0000 |
| 14.0000 | 17.0000 | 0.0095 | 0.0810 | 1.0100 | 1.0000 |
| 11.0000 | 24.0000 | 0.0070 | 0.0560 | 0.7450 | 1.0000 |
| 11.0000 | 4.0000 | 0.0018 | 0.0139 | 0.2080 | 1.0000 |
| 11.0000 | 15.0000 | 0.0049 | 0.0416 | 0.5210 | 1.0000 |
| 15.0000 | 25.0000 | 0.0034 | 0.0292 | 0.0355 | 1.0000 |
| 15.0000 | 26.0000 | 0.0049 | 0.0419 | 0.5240 | 1.0000 |
| 26.0000 | 5.0000 | 0.0090 | 0.0070 | 0.1040 | 1.0000 |
| 4.0000 | 21.0000 | 0.0023 | 0.0190 | 0.2390 | 1.0000 |
| 2.0000 | 21.0000 | 0.0011 | 0.0088 | 0.1710 | 1.0000 |
| 1.0000 | 23.0000 | 0.0022 | 0.0172 | 0.2570 | 1.0000 |
| 29.0000 | 14.0000 | 0.0070 | 0.0599 | 0.7480 | 1.0000 |
| 14.0000 | 30.0000 | 0.0029 | 0.0246 | 0 | 1.0000 |
| 10.0000 | 12.0000 | 0.0049 | 0.0341 | 0.5210 | 1.0000 |
| 11.0000 | 2.0000 | 0.0022 | 0.0190 | 0.2390 | 1.0000 |
| 15.0000 | 3.0000 | 0.0090 | 0.0070 | 1.0400 | 1.0000 |
| 8.0000 | 18.0000 | 0.0025 | 0.0195 | 0.1040 | 1.0000 |
| 9.0000 | 24.0000 | 0.0022 | 0.0172 | 0.2570 | 1.0000 |
| 19.0000 | 17.0000 | 0.0049 | 0.0416 | 0.5210 | 1.0000 |
| 20.0000 | 23.0000 | 0.0022 | 0.0172 | 0.2570 | 1.0000 |
| 27.0000 | 26.0000 | 0.0087 | 0.0742 | 0.9270 | 1.0000 |

>> lfybus
 >> lfnewton
 >> busout

3.0 Data Analysis, Preparation and Keying into Computer

(a) Bus Data File or Bus Data

The rest of this work was done by using a computer. The format for the bus entry was chosen so that the data required for each bus would be entered in a single row in computer [4]. In the bus data or matrix, column 1 is the bus number. Column 2 is the bus code, column 3 and 4 are voltage magnitudes in p.u and phase angles in degrees. Column 5 and 6 are loads in MW and Mvar column 7 through 10 are MW, Mvar, MinMvar and maxMvar of generation. The last column is the injected reactive power (Mvar) of shunt capacitor or reactor. Then for the bus code entered in column 2 [4]:

- 1 represents the slack bus
- 2 represents the voltage controlled bus, while
- 0 represents the load bus

Next, the bus data or matrix required for each bus were keyed in a square bracket row by row, of course, separating each row with a semi-colon and entered in MATLAB prompt or workspace (see table 5 and the output results).

Table 5: Keyed Bus Data and Output

Warning: Could not get change notification handle for local d:\.
 Performance degradation may occur due to on-disk directory change checking.

To get started, select "MATLAB Help" from the Help menu.

```
>> clear %clears all variable from workspace
>> basemva=100; accuracy=0.001; accel=1.8; maxiter=100;
>> busdata=[1 1 1.02 0 0 0 0 0 0 0;2 2 1 0 4 -10 0 0 0 0;3 2 1.04 0 0 0 300 40 0
110 0;4 2 1 0 140 30 0 0 0 0;5 2 1 0 90 30 0 0 0 0; 6 2 1.04 0 160 70 20 0 0 0
0;7 2 1 0 0 0 400 60 0 0 0;8 2 1 0 150 70 0 0 0 140 0;9 2 1 0 300 90 0 0 0 0;10 0
1.02 0 120.37 61.65 0 0 0 0 19;11 0 1 0 160.56 82.24 150 50 0 114 0;12 0 1 0 334
171.11 0 0 0 0 0;13 0 1 0 176.65 90.49 0 0 0 0;14 0 1 0 82.23 42.129 0 0 0 0;15
0 1 0 130.51 66.86 0 0 0 0;16 0 1 0 233.379 119.56 0 0 0 0;17 0 1 0 74.48 38.14
0 0 0 0 0;18 0 1.03 0 200 102.44 280 45 0 100 0;19 0 1 0 10 5.11 0 0 0 0;20 0 1 0
0 0 0 0 0;21 0 1.02 0 47.997 24.589 240 55 0 104 0;22 0 1.05 0 252.45 129.330
700 68 0 108 0;23 0 1 0 119.99 61.477 0 0 0 0;24 0 1.04 0 63.22 32.38 180 0 0 132
4.3;25 0 1 0 113.05 57.91 0 0 0 0;26 0 1.01 0 163.95 83.9 190 -35 0 126 0;27 0
1.03 0 7.44 3.790 150 51 0 100 0;28 0 1.02 0 69.99 35.85 130 80 0 150 0;29 0 1 0
149.77 76.72 0 0 0 0;30 0 1 0 73.07 37.43 0 0 0 0]
```

| busdata = | | | | | | | |
|------------|-----------|--------|---|----------|----------|----------|----------|
| 1.0000 | 1.0000 | 1.0200 | 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 4.0000 | -10.0000 | 0 | 0 |
| 2.0000 | 2.0000 | 1.0000 | 0 | 0 | 0 | 300.0000 | 40.0000 |
| 0 | 0 | 0 | 0 | 140.0000 | 30.0000 | 0 | 0 |
| 3.0000 | 2.0000 | 1.0400 | 0 | 90.0000 | 30.0000 | 0 | 0 |
| 0 110.0000 | 0 | 0 | 0 | 160.0000 | 70.0000 | 20.0000 | 0 |
| 4.0000 | 2.0000 | 1.0000 | 0 | 0 | 0 | 400.0000 | 60.0000 |
| 0 | 0 | 0 | 0 | 150.0000 | 70.0000 | 0 | 0 |
| 5.0000 | 2.0000 | 1.0000 | 0 | 300.0000 | 90.0000 | 0 | 0 |
| 0 | 0 | 0 | 0 | 120.3700 | 61.6500 | 0 | 0 |
| 6.0000 | 2.0000 | 1.0400 | 0 | 160.5600 | 82.2400 | 150.0000 | 50.0000 |
| 0 | 0 | 0 | 0 | 334.0000 | 171.1100 | 0 | 0 |
| 7.0000 | 2.0000 | 1.0000 | 0 | 176.6500 | 90.4900 | 0 | 0 |
| 0 | 0 | 0 | 0 | 82.2300 | 42.1290 | 0 | 0 |
| 8.0000 | 2.0000 | 1.0000 | 0 | 130.5100 | 66.8600 | 0 | 0 |
| 0 140.0000 | 0 | 0 | 0 | 233.3790 | 119.5600 | 0 | 0 |
| 9.0000 | 2.0000 | 1.0000 | 0 | 74.4800 | 38.1400 | 0 | 0 |
| 0 | 0 | 0 | 0 | 200.0000 | 102.4400 | 280.0000 | 45.0000 |
| 10.0000 | 0 | 1.0200 | 0 | 10.0000 | 5.1100 | 0 | 0 |
| 0 | 0 19.0000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11.0000 | 0 | 1.0000 | 0 | 47.9970 | 24.5890 | 240.0000 | 55.0000 |
| 0 114.0000 | 0 | 0 | 0 | 252.4500 | 129.3300 | 700.0000 | 68.0000 |
| 12.0000 | 0 | 1.0000 | 0 | 119.9900 | 61.4770 | 0 | 0 |
| 0 | 0 | 0 | 0 | 63.2200 | 32.3800 | 180.0000 | 0 |
| 13.0000 | 0 | 1.0000 | 0 | 113.0500 | 57.9100 | 0 | 0 |
| 0 | 0 | 0 | 0 | 163.9500 | 83.9000 | 190.0000 | -35.0000 |
| 14.0000 | 0 | 1.0000 | 0 | 7.4400 | 3.7900 | 150.0000 | 51.0000 |
| 0 | 0 | 0 | 0 | 69.9900 | 35.8500 | 130.0000 | 80.0000 |
| 15.0000 | 0 | 1.0000 | 0 | 149.7700 | 76.7200 | 0 | 0 |
| 0 | 0 | 0 | 0 | 73.0700 | 37.4300 | 0 | 0 |
| 16.0000 | 0 | 1.0000 | 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17.0000 | 0 | 1.0000 | 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18.0000 | 0 | 1.0300 | 0 | 0 | 0 | 0 | 0 |
| 0 100.0000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 19.0000 | 0 | 1.0000 | 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 20.0000 | 0 | 1.0000 | 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 21.0000 | 0 | 1.0200 | 0 | 0 | 0 | 0 | 0 |
| 0 104.0000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 22.0000 | 0 | 1.0500 | 0 | 0 | 0 | 0 | 0 |
| 0 108.0000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 23.0000 | 0 | 1.0000 | 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 24.0000 | 0 | 1.0400 | 0 | 0 | 0 | 0 | 0 |
| 0 132.0000 | 4.3000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 25.0000 | 0 | 1.0000 | 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 26.0000 | 0 | 1.0100 | 0 | 0 | 0 | 0 | 0 |
| 0 126.0000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 27.0000 | 0 | 1.0300 | 0 | 0 | 0 | 0 | 0 |
| 0 100.0000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 28.0000 | 0 | 1.0200 | 0 | 0 | 0 | 0 | 0 |
| 0 150.0000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 29.0000 | 0 | 1.0000 | 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 30.0000 | 0 | 1.0000 | 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

(b) Line Data File or Line Data

Similarly, the line data were prepared, keyed in and 'entered' in MATLAB workspace. The line data were handled by using the line bus numbers, the line resistance R, the line reactance X, one half of the total line charging susceptance y/2 and the transformer tap-settings denoted by (1). The output result of the keyed line data in square bracket is shown in Table 6.

Table 6: Keyed Line Data and Output.

```
> %linedata
> linedata=[16 12 0.0006 0.0051 0.065 1;12 1 0.0022 0.0172 0.257 1;12 11 0.0101
.0799 1.162 1;12 13 0.0049 0.0416 0.521 1;13 10 0.0041 0.0349 0.437 1;10 11 0.0089
.0763 0.954 1;10 27 0.0056 0.477 0.597 1;12 6 0.0056 0.477 0.597 1;27 8 0.0087
.0742 0.927 1;27 7 0.0022 0.0246 0.308 1;7 28 0.0111 0.9420 1.178 1;8 29 0.0034
.0292 0.364 1;29 22 0.0082 0.0899 0.874 1;14 17 0.0095 0.0810 1.010 1;11 24 0.0070
.0560 0.745 1;11 4 0.0018 0.0139 0.208 1;11 15 0.0049 0.0416 0.521 1;15 25 0.0034
.0292 0.0355 1;15 26 0.0049 0.0419 0.524 1;26 5 0.009 0.007 0.104 1;4 21 0.0023
.0190 0.239 1;2 21 0.0011 0.0088 0.171 1;1 23 0.0022 0.0172 0.257 1;29 14 0.007
.0599 0.748 1;14 30 0.0029 0.0246 0 1;10 12 0.0049 0.0341 0.521 1;11 2 0.0022 0.019
.239 1;15 3 0.009 0.007 1.04 1;8 18 0.0025 0.0195 0.104 1;9 24 0.0022 0.0172 0.257
:19 17 0.0049 0.0416 0.521 1;20 23 0.0022 0.0172 0.257 1;27 26 0.0087 0.0742 0.927]
```

```
inedata =
```

| | | | | | |
|---------|---------|--------|--------|--------|--------|
| 16.0000 | 12.0000 | 0.0006 | 0.0051 | 0.0650 | 1.0000 |
| 12.0000 | 1.0000 | 0.0022 | 0.0172 | 0.2570 | 1.0000 |
| 12.0000 | 11.0000 | 0.0101 | 0.0799 | 1.1620 | 1.0000 |
| 12.0000 | 13.0000 | 0.0049 | 0.0416 | 0.5210 | 1.0000 |
| 13.0000 | 10.0000 | 0.0041 | 0.0349 | 0.4370 | 1.0000 |
| 10.0000 | 11.0000 | 0.0089 | 0.0763 | 0.9540 | 1.0000 |
| 10.0000 | 27.0000 | 0.0056 | 0.4770 | 0.5970 | 1.0000 |
| 12.0000 | 6.0000 | 0.0056 | 0.4770 | 0.5970 | 1.0000 |
| 27.0000 | 8.0000 | 0.0087 | 0.0742 | 0.9270 | 1.0000 |
| 27.0000 | 7.0000 | 0.0022 | 0.0246 | 0.3080 | 1.0000 |
| 7.0000 | 28.0000 | 0.0111 | 0.9420 | 1.1780 | 1.0000 |
| 8.0000 | 29.0000 | 0.0034 | 0.0292 | 0.3640 | 1.0000 |
| 29.0000 | 22.0000 | 0.0082 | 0.0899 | 0.8740 | 1.0000 |
| 14.0000 | 17.0000 | 0.0095 | 0.0810 | 1.0100 | 1.0000 |
| 11.0000 | 24.0000 | 0.0070 | 0.0560 | 0.7450 | 1.0000 |
| 11.0000 | 4.0000 | 0.0018 | 0.0139 | 0.2080 | 1.0000 |
| 11.0000 | 15.0000 | 0.0049 | 0.0416 | 0.5210 | 1.0000 |
| 15.0000 | 25.0000 | 0.0034 | 0.0292 | 0.0355 | 1.0000 |
| 15.0000 | 26.0000 | 0.0049 | 0.0419 | 0.5240 | 1.0000 |
| 26.0000 | 5.0000 | 0.0090 | 0.0070 | 0.1040 | 1.0000 |
| 4.0000 | 21.0000 | 0.0023 | 0.0190 | 0.2390 | 1.0000 |
| 2.0000 | 21.0000 | 0.0011 | 0.0088 | 0.1710 | 1.0000 |
| 1.0000 | 23.0000 | 0.0022 | 0.0172 | 0.2570 | 1.0000 |
| 29.0000 | 14.0000 | 0.0070 | 0.0599 | 0.7480 | 1.0000 |
| 14.0000 | 30.0000 | 0.0029 | 0.0246 | 0 | 1.0000 |
| 10.0000 | 12.0000 | 0.0049 | 0.0341 | 0.5210 | 1.0000 |
| 11.0000 | 2.0000 | 0.0022 | 0.0190 | 0.2390 | 1.0000 |
| 15.0000 | 3.0000 | 0.0090 | 0.0070 | 1.0400 | 1.0000 |
| 8.0000 | 18.0000 | 0.0025 | 0.0195 | 0.1040 | 1.0000 |
| 9.0000 | 24.0000 | 0.0022 | 0.0172 | 0.2570 | 1.0000 |
| 19.0000 | 17.0000 | 0.0049 | 0.0416 | 0.5210 | 1.0000 |
| 20.0000 | 23.0000 | 0.0022 | 0.0172 | 0.2570 | 1.0000 |
| 27.0000 | 26.0000 | 0.0087 | 0.0742 | 0.9270 | 1.0000 |

```
>> lfybus
>> lfnnewton
>> busout
```

4.0 Load Flow Studies Using Newton-Raphson’s Solution Method

Now, with the output results of the bus and the line data still in MATLAB workspace in the computer, a command program called “lf newton” was employed and ‘entered’ in MATLAB prompt to obtain the power solution by Newton Raphson’s method. Table 7 and 8 are the finding output results.

Table 7: Power Flow Solution by Newton Raphson’s method

```

Power Flow Solution by Newton-Raphson Method
Maximum Power Mismatch = 7.16159e-006
No. of Iterations = 10
    
```

| Bus No. | Voltage Mag. | Angle Degree | -----Load----- | | ---Generation--- | | Injected |
|---------|--------------|--------------|----------------|----------|------------------|-----------|----------|
| | | | MW | Mvar | MW | Mvar | Mvar |
| 1 | 1.020 | 0.000 | 0.000 | 0.000 | 822.324 | -128.009 | 0.000 |
| 2 | 1.000 | -1.822 | 4.000 | -10.000 | 0.000 | -276.417 | 0.000 |
| 3 | 1.090 | 5.248 | 0.000 | 0.000 | 300.000 | -16.914 | 0.000 |
| 4 | 1.000 | -2.731 | 140.000 | 30.000 | 0.000 | -249.589 | 0.000 |
| 5 | 1.000 | 11.988 | 90.000 | 30.000 | 0.000 | -91.000 | 0.000 |
| 6 | 1.040 | -45.880 | 160.000 | 70.000 | 20.000 | 61.090 | 0.000 |
| 7 | 1.000 | 33.326 | 0.000 | 0.000 | 400.000 | -201.357 | 0.000 |
| 8 | 1.050 | 23.639 | 150.000 | 70.000 | 0.000 | -826.764 | 0.000 |
| 9 | 1.000 | -11.322 | 300.000 | 90.000 | 0.000 | 11.443 | 0.000 |
| 10 | 1.055 | -6.891 | 120.370 | 61.650 | 0.000 | 0.000 | 19.000 |
| 11 | 1.031 | -2.775 | 160.560 | 82.240 | 150.000 | 50.000 | 0.000 |
| 12 | 1.022 | -6.724 | 334.000 | 171.110 | 0.000 | 0.000 | 0.000 |
| 13 | 1.038 | -8.611 | 176.650 | 90.490 | 0.000 | 0.000 | 0.000 |
| 14 | 1.618 | 16.163 | 82.230 | 42.129 | 0.000 | 0.000 | 0.000 |
| 15 | 1.058 | 4.682 | 130.510 | 66.860 | 0.000 | 0.000 | 0.000 |
| 16 | 1.015 | -7.345 | 233.379 | 119.560 | 0.000 | 0.000 | 0.000 |
| 17 | 1.913 | 13.636 | 74.480 | 38.140 | 0.000 | 0.000 | 0.000 |
| 18 | 1.043 | 24.515 | 200.000 | 102.440 | 280.000 | 45.000 | 0.000 |
| 19 | 1.954 | 13.427 | 10.000 | 5.110 | 0.000 | 0.000 | 0.000 |
| 20 | 1.025 | -1.192 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 21 | 1.006 | -1.482 | 47.997 | 24.589 | 240.000 | 55.000 | 0.000 |
| 22 | 1.329 | 35.784 | 252.450 | 129.330 | 700.000 | 68.000 | 0.000 |
| 23 | 1.020 | -1.159 | 119.990 | 61.477 | 0.000 | 0.000 | 0.000 |
| 24 | 1.017 | -8.479 | 63.220 | 32.380 | 180.000 | 0.000 | 4.300 |
| 25 | 1.039 | 3.058 | 113.050 | 57.910 | 0.000 | 0.000 | 0.000 |
| 26 | 1.016 | 11.782 | 163.950 | 83.900 | 190.000 | -35.000 | 0.000 |
| 27 | 1.048 | 26.916 | 7.440 | 3.790 | 150.000 | 51.000 | 0.000 |
| 28 | -0.734 | 704.358 | 69.990 | 35.850 | 130.000 | 80.000 | 0.000 |
| 29 | 1.274 | 22.304 | 149.770 | 76.720 | 0.000 | 0.000 | 0.000 |
| 30 | 1.611 | 15.792 | 73.070 | 37.430 | 0.000 | 0.000 | 0.000 |
| Total | | | 3427.106 | 1603.105 | 3562.324 | -1403.517 | 23.300 |

>> lineflow

Table 8: Line Flow and Losses

| Line Flow and Losses | | | | | | |
|----------------------|--------------------------|----------|---------|---------------|-------------|-----|
| --Line-- | Power at bus & line flow | | | --Line loss-- | Transformer | |
| from to | MW | Mvar | MVA | MW | Mvar | tap |
| 1 | 822.324 | -128.009 | 832.228 | | | |
| 12 | 702.008 | -84.789 | 707.110 | 10.492 | 28.465 | |
| 23 | 120.317 | -43.219 | 127.844 | 0.312 | -51.059 | |
| 2 | -4.000 | -266.417 | 266.447 | | | |
| 21 | -74.498 | -71.440 | 103.217 | 0.094 | -33.644 | |
| 11 | 70.498 | -194.977 | 207.331 | 0.753 | -42.804 | |
| 3 | 300.000 | -16.914 | 300.476 | | | |
| 15 | 300.000 | -16.914 | 300.476 | 7.679 | -234.099 | |
| 4 | -140.000 | -279.589 | 312.682 | | | |
| 11 | -22.909 | -241.547 | 242.631 | 0.887 | -36.067 | |
| 21 | -117.091 | -38.042 | 123.116 | 0.320 | -45.426 | |
| 5 | -90.000 | -121.000 | 150.801 | | | |
| 26 | -90.000 | -121.000 | 150.801 | 1.830 | -19.709 | |
| 6 | -140.000 | -8.910 | 140.283 | | | |
| 12 | -140.000 | -8.910 | 140.283 | 1.175 | -26.785 | |
| 7 | 400.000 | -201.357 | 447.822 | | | |
| 27 | 456.882 | -241.506 | 516.784 | 5.569 | -2.377 | |
| 28 | -56.882 | 40.150 | 69.624 | 3.128 | 84.300 | |
| 8 | -150.000 | -896.764 | 909.222 | | | |
| 27 | -83.118 | -87.673 | 120.811 | 0.562 | -199.288 | |
| 29 | 12.922 | -845.276 | 845.374 | 19.997 | 72.541 | |
| 18 | -79.804 | 36.185 | 87.624 | 0.196 | -21.255 | |
| 9 | -300.000 | -78.557 | 310.115 | | | |
| 24 | -300.000 | -78.557 | 310.115 | 2.041 | -36.318 | |
| 10 | -120.370 | -42.650 | 127.703 | | | |
| 13 | 99.197 | -6.374 | 99.402 | 0.428 | -92.122 | |
| 11 | -96.698 | -57.667 | 112.588 | 0.936 | -199.669 | |
| 27 | -128.564 | -24.203 | 130.822 | 0.921 | -53.670 | |
| 12 | 5.695 | 45.594 | 45.949 | 0.474 | -109.120 | |
| 11 | -10.560 | -32.240 | 33.925 | | | |
| 12 | 91.279 | -119.789 | 150.603 | 0.793 | -238.559 | |
| 10 | 97.634 | -142.003 | 172.329 | 0.936 | -199.669 | |
| 24 | 187.588 | -67.322 | 199.302 | 2.326 | -137.642 | |
| 4 | 23.796 | 205.479 | 206.853 | 0.887 | -36.067 | |
| 15 | -341.111 | -60.778 | 346.483 | 5.364 | -68.217 | |
| 2 | -69.745 | 152.173 | 167.395 | 0.753 | -42.804 | |
| 12 | -334.000 | -171.110 | 375.279 | | | |
| 16 | 233.771 | 109.414 | 258.109 | 0.392 | -10.146 | |
| 1 | -691.516 | 113.254 | 700.728 | 10.492 | 28.465 | |
| 11 | -90.486 | -118.770 | 149.311 | 0.793 | -238.559 | |
| 13 | 78.277 | -102.419 | 128.906 | 0.396 | -107.161 | |
| 6 | 141.175 | -17.876 | 142.302 | 1.175 | -26.785 | |
| 10 | -5.221 | -154.714 | 154.803 | 0.474 | -109.120 | |
| 13 | -176.650 | -90.490 | 198.478 | | | |
| 12 | -77.881 | -4.742 | 78.025 | 0.396 | -107.161 | |
| 10 | -98.769 | -85.748 | 130.798 | 0.428 | -92.122 | |
| 14 | -82.230 | -42.129 | 92.394 | | | |
| 17 | 98.313 | -862.755 | 868.338 | 13.349 | -520.325 | |
| 29 | -253.688 | 782.557 | 822.650 | 27.320 | -83.358 | |
| 30 | 73.145 | 38.069 | 82.459 | 0.075 | 0.639 | |
| 15 | -130.510 | -66.860 | 146.639 | | | |
| 11 | 346.475 | -7.439 | 346.555 | 5.364 | -68.217 | |
| 25 | 113.545 | 54.347 | 125.881 | 0.495 | -3.563 | |
| 26 | -298.209 | 103.417 | 315.632 | 5.039 | -69.686 | |
| 3 | -292.321 | -217.185 | 364.171 | 7.679 | -234.099 | |

| | | ky | | | | | |
|------------|----|----------|----------|---------|------------------|----------|--|
| 16 | | -233.379 | -119.560 | 262.222 | | | |
| | 12 | -233.379 | -119.560 | 262.222 | 0.392 | -10.146 | |
| 17 | | -74.480 | -38.140 | 83.678 | | | |
| | 14 | -84.964 | 342.430 | 352.813 | 13.349 | -520.325 | |
| | 19 | 10.484 | -380.570 | 380.715 | 0.484 | -385.680 | |
| 18 | | 80.000 | -57.440 | 98.485 | | | |
| | 8 | 80.000 | -57.440 | 98.485 | 0.196 | -21.255 | |
| 19 | | -10.000 | -5.110 | 11.230 | | | |
| | 17 | -10.000 | -5.110 | 11.230 | 0.484 | -385.680 | |
| 20 | | 0.000 | 0.000 | 0.000 | | | |
| | 23 | -0.000 | -0.000 | 0.000 | 0.015 | -53.637 | |
| 21 | | 192.003 | 30.411 | 194.396 | | | |
| | 4 | 117.411 | -7.384 | 117.643 | 0.320 | -45.426 | |
| | 2 | 74.592 | 37.795 | 83.621 | 0.094 | -33.644 | |
| 22 | | 447.550 | -61.330 | 451.733 | | | |
| | 29 | 447.550 | -61.330 | 451.733 | 9.697 | -189.952 | |
| 23 | | -119.990 | -61.477 | 134.822 | | | |
| | 1 | -120.005 | -7.840 | 120.261 | 0.312 | -51.059 | |
| | 20 | 0.015 | -53.637 | 53.637 | 0.015 | -53.637 | |
| 24 | | 116.780 | -28.080 | 120.109 | | | |
| | 11 | -185.261 | -70.319 | 198.158 | 2.326 | -137.642 | |
| | 9 | 302.041 | 42.239 | 304.981 | 2.041 | -36.318 | |
| 25 | | -113.050 | -57.910 | 127.019 | | | |
| | 15 | -113.050 | -57.910 | 127.019 | 0.495 | -3.563 | |
| 26 | | 26.050 | -118.900 | 121.720 | | | |
| | 15 | 303.248 | -173.103 | 349.176 | 5.039 | -69.686 | |
| | 5 | 91.830 | 101.291 | 136.721 | 1.830 | -19.709 | |
| | 27 | -369.028 | -47.088 | 372.020 | 11.680 | -97.925 | |
| 27 | | 142.560 | 47.210 | 150.174 | | | |
| | 10 | 129.485 | -29.467 | 132.795 | 0.921 | -53.670 | |
| | 8 | 83.680 | -111.615 | 139.500 | 0.562 | -199.288 | |
| | 7 | -451.313 | 239.129 | 510.750 | 5.569 | -2.377 | |
| | 26 | 380.708 | -50.837 | 384.087 | 11.680 | -97.925 | |
| 28 | | 60.010 | 44.150 | 74.501 | | | |
| | 7 | 60.010 | 44.150 | 74.501 | 3.128 | 84.300 | |
| 29 | | -149.770 | -76.720 | 168.277 | | | |
| | 8 | 7.074 | 917.817 | 917.844 | 19.997 | 72.541 | |
| | 22 | -437.853 | -128.622 | 456.354 | 9.697 | -189.952 | |
| | 14 | 281.009 | -865.915 | 910.371 | 27.320 | -83.358 | |
| 30 | | -73.070 | -37.430 | 82.099 | | | |
| | 14 | -73.070 | -37.430 | 82.099 | 0.075 | 0.639 | |
| Total loss | | | | | 135.219-2983.320 | | |

4.1 Analysis Result

The results obtained in Table 7 showed that all the bus voltages outside the statutory limit of $0.95 \leq V_i \leq 1.05$ p.u are: bus 14 (Jos) with value of 0.9359 p.u, bus 17 (Gombe) 0.9175 p.u, bus 19 (Maiduguri) 0.9106 p.u, bus 22 (Kano) 0.8849 p.u, bus 28 (Berni-Kebbi) -0.734 p.u, bus 3 (Okpai) 1.090 p.u and bus 29 (Kaduna) 0.9880 p.u while bus 30 (Makurdi) gave the value 0.8247 p.u under normal uncompensated condition.

These problems can be arrested either by the use of dynamic static var compensator (SVC) or supplementary Fuzzy Controller Static Var Compensator (FCSVC). The obvious rise in voltages even at the most remote buses from the national control centre (NCC) egKano, Maiduguri and Makurdi may be due to poor reactive power management in the system, faults and constant system breakdown due to aging equipment.

The result in Table 8 showed a total active power loss of 135.219MW which is bound to reduce with the application of a proper form of compensation in the system.

5.0 Conclusion

Load flow studies is a rudimental framework that should be carried out before any form of compensation is applied for arresting constant system breakdown and outage in a transmission network.

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